

#105181 GYRE 80-6A

GYRE (#80014)

W. Florida Shelf

June 14-July 5, 1980

C.Holmes/F. Manheim

SAMPLE/GEOCHEM LOG

80014/09

GYRE

80-6A

~~6-80~~

LOG BOOK

#80014

105181

Malg² 2114-0016 500ml square wide
mouth bottles.



ACCOUNT BOOK

10 IN. x 8 1/4 IN. (25.4 cm x 20.9 cm)

AVAILABLE AS:

No. 64-6118 (168-150-R) 150 pages

No. 64-6138 (168-300-R) 300 pages

RULING:

Record Ruled

Record Ruled

MADE IN U.S.A.

VERNON McMILLAN, Inc., ELIZABETH, N.J. 07208

GYRE 80-6A #80014

14 June 80,

Depart New Orleans 1630

Out of Mississippi ~2400

15 June 80

acoustics with 3.5 MHz sounder
streaming 800 joule mini speaker for seismic
profiling.

~~Receiving~~ Watcher monitors navigation
and 3.5 and speaker.

Set up ~~phosphorus~~ phosphorus test
for phosphorite indication:

20% HNO_3 ~ 10 seconds with sample
1 drop ~~an~~ saturated ammonium
molybdate as indicator. Bright
yellow indication with phosphate
rock standard (NBS) in spot
plate.

Box Core: Found Driscoll (URI) had
sent totally different cores
than we had expected. Boxes
are ~ 18" x 5". However each box
is different in exact dimensions.
In order to sample, Theo. has made
up a sheet metal cap for the bottom
so we can move the box.

For C14 this section, our original plates are not big enough. Therefore we will make up a separate set of plates for each box using $\frac{1}{8}$ " plexiglass which Theo has supplied (personal).

LAB: Cut down syringes for a squeezer and put gaskets on screens.

16 June 80

~~15th~~

SAMPLE

G-6-80-I(cc)

15th station - Piston Core

G-6-80-I-cc

Lat. $28^{\circ}59.79'$ Long. $88^{\circ}05.94'$

Time 0925 1270 meters

S 35.2‰

PO₄-trace

29 foot core

core catcher sampled by Frank

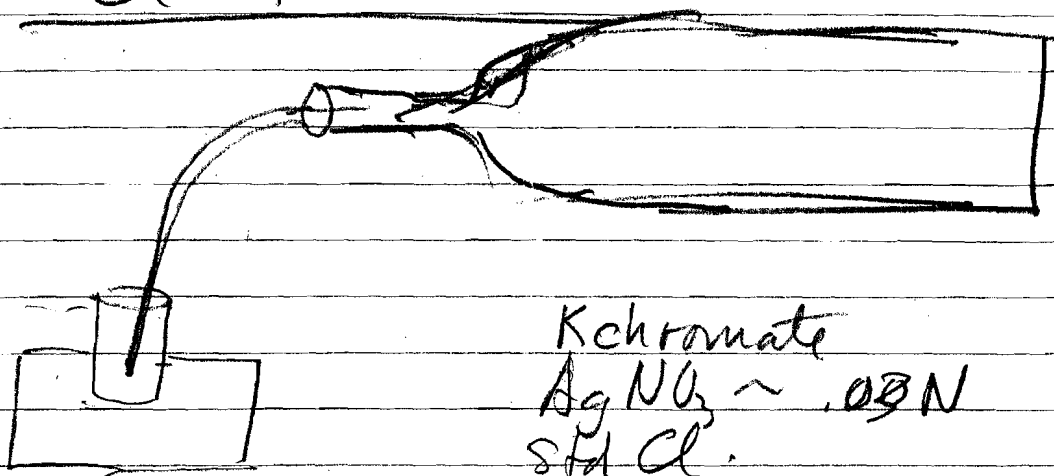
① Paleo ② Pore water ③ Chem.

~~Box 10000~~

Cl⁻ Titration:

Frank suggests using a fine stream of propane to stir samples.

Cl. Titration



1. Pipette solutions [Accurate]
2. Add dist water + KCr
3. Fill burette
4. Titrate.
5. Check blank
6. Include standards

Pore water:
salinity (in part.) 35.2 ‰

PO₄ - Trace

Box Core: Decided to make 3 sided box made out of sheet metal plates that we brought. This will be used to sub sample the main box. Test core rig - Tripped OK, but there is a question about enough weight to penetrate and if the swing of the scoop will lift the cover out of the sediment.

Chem.: Cl^- - made up saturated soln. of AgNO_3 to be used to provide a consistent source of AgNO_3 for titration. This will be a trial and error technique until the proper dilution is found to approximate .05 N.

Found that T.A.M. has an oxygen titration apparatus in the electronics lab. containing a small magnetic stirrer and a buret clamp. We will "borrow" these for the cruise.

Found that small pieces of $\frac{1}{8}$ " nails would work as stir bar. Have to check with Frank about metal in the titration, can ~~expose~~ epoxy if necessary. - Frank sealed one in polyethylene, works fine.

Watch: Piston core set up for second

~~station~~ station, ready to go at ~ 0400
Tomorrow.

17 June 80

Piston Core / STA. 2 - Sampled core catcher
split for pore water, P and forams.
P = 0 ; S = 34.4900

START Phosphate Stations

P-1 Box Core - 1 $29^{\circ}20'0''$ x $87^{\circ}43'2''$ depth 170m

sub sampled - thin sections every 2 cm to
18 cm then 18-26 cm Tot 26 cm.

~~Samples~~ ~~from~~

0-2 cm fine brown sand

2-28 cm shell sand

13 samples

18-26 cm fine clay sand

preliminary P = 0

STA. P-2 $29^{\circ}20'0''$ x $87^{\circ}43'2''$ depth —

Box Core - ~~panned~~ scoop jammed against
box, then believe cover pull out of sediment
when the scoop was closing. Changed box.

Smith-McIntyre grab sample -

Large chunk of coral ~~core~~ caught in
jaws - good grab. - fine sand
prelim. P = 0

STA. P-3 ^{29°26'} ~~29°26'~~ x 87°35' Smith-MacIntyre Grab
 sm-1 75 m - didn't trigger

sm-2 81 m - ^(75m) well washed coral fragments
 with a few fines
 prelin. P=0

Sparker
 Transect

STA. P-4 ^(37m) 29°40.5' x 87°37' Box Core
 10 cm of gray sand. with well preserved surface
 of brown material + shell + debris
 sub sampled 0-2 cm, 2-8 and 8-10 cm
 prelin. P=0

STA. P-5 ^(110m) 29°35.5' x 87°20.5' Box Core
 14 cm light shell sand, most of surface
 washed away.

Entire box sampled:

0-4 cm, 4-9 cm and 9-14 cm.

Forger Tried gravity core - no luck

End of Frank's Line

Start on piston core near transects
 tomorrow. Will have two core crew on
 8 hour watches ^{while} ~~with~~ the rest mind the
 ship 4 hours at a time.

Talked to Theo about Dredges. He
~~also~~ said they're clam dredges and

not worth a piece of shit. However we'll drag them out between the ~~core~~ piston core transect and the first drill Test.

Chen Lab:

STA-2 Ray doing some real fine work. Picked out the "mysterious ~~orange~~ orange specs" to have S.E.M probe analysis of Phosphate ~~done~~ done.

Will finish up P analysis on all our samples.

P routine:

4 sub samples (scoop)
2 aliquots of each sample
one ~~aliquot~~ aliquot rinsed with D.W. and water pulled out of spot with wipette wick.

acidify with 20% HNO_3 dropwise until carbonate fizz is relaxed. Add more acid then saturated ammonium molybdate solution.

Watch Streaming speaker on transect to core site.

18 June 80

Watch - Spiked sediment from Box Core of STA. P-1 with Phosphate Rock. ~ 5%, 10% and 15% → ~ 1, 2 and 3% P. Good color reaction with molybdate addition, but not necessary in white precipitate region due to the lack of gradual phosphate. Will watch for color deepening in routine analysis, especially those samples high in glauconite which give a yellow tint when reacted with the acid.

Frank says that he has checked all of the samples for P - so that's that.

Chem:

Filtered AgNO_3 - would not saturate so indicating it as concentrated (very!).
~~made~~

K_2CrO_4 - made up ~ 5% solution by covering bottom of 25 ml vial with reagent and filling bottle $\frac{1}{2}$ way. Add 1 drop of conc. AgNO_3 → red ppt., filtered.

Trial Titration

AgNO_3 1 ml conc in 50 ml D.W.

Sea water 0.5 ml

1 drop ~~conc~~ Cr_2O_4

Too concentrated - 3 drop to eq. = no sensitivity

✓ Done ✓

Core 8 cc 3 = 35.3

Tried 10 fold dilution of $\text{AgNO}_3 \rightarrow 1/500 = \text{too dilute}$
 Will try $.5/50 = 1/100$ dilution.

Epoxyed nails for stir bars. OK.

see P.25
 for location

Piston Core Stations 3-7 Larry Doyle
 line #1.

Samples from core catcher for pore water
 and bag testing.

19 June 80

see P. 25
for Location

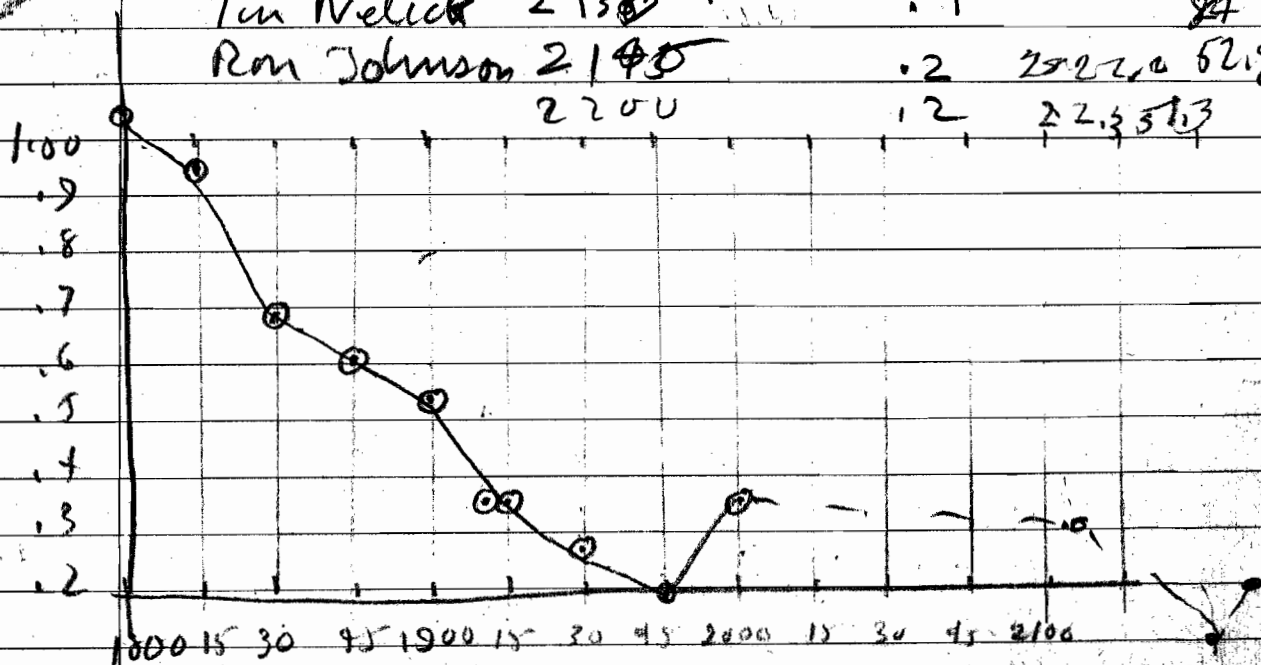
Piston Core Stations 8-11 and line #1
sampled catcher for pore water and forams

on the drill test site, ~ 1100 h

		T°C	
Salinities		Thermistor	Thermom
	1737		32.3
	1750	30.0?	32.4
	1805	29.0	32.4
	1837	27.8	32.8
	1852	26.3°	32.6-1
	1909	27.0	28.1 32.8
	1937		28.0 32.6
	2005		27.8 32.4
Water blue, with Sargassum weed			
	2034		27.9 32.4
	2104		28.1 32.7

Cable Coordinate Course Vector 1 hr
Set's drift

		<u>X</u>	<u>Y</u> set's drift
			N-NW set
1800			1.04 towards S-SE
1815			.85
1830	28°	17.86.88	11.25
1845		18.28	9.87
1900		18.7	8.57
1910		18.3	7.66
1915		18.19	7.22
1930		18.7	5.83
1945		20.2	4.44
2000		20.71	3.08
2115		21.8	0.7
Tim Velick 2130			.1
Ron Johnson 2145			.2
2200			.2



Check water sample for Loop current and found a surprising low salinity: began water testing ~ early 1/2 hour.

Procedure: Water sample in bucket, ~~then~~ take temp., record position and time (MGT) ~~Salinity~~ in and depth. Salinity is taken first with the refractometer and then after temperature equilibration run on the Bissonet + Bernon Salinometer calibrated with IAPSO std. sea water σ_t 19.376.

G.M.T	Time	S_R	S_S	$T^\circ C$	Loc	Depth	
						depth	m
4/19	1737	32.3	32.86	—	28° 16.9' x 85° 15.5'		
	1750	32.4	32.84	—	17.0' x	14.9	
	1805	32.4	32.83	—	17.3' x	13.3	
	1837	32.8	32.85	—	18.1' x	10.3	
	1855	32.7	32.88	—	18.6' x	09.0	
	1909	32.8	32.86	28.1	19.0 x	07.7	
	1937	32.6	32.81	28.0	20.0' x	05.1	
	2005	32.4	32.72	27.8	20.9' x	02.4	150
	2034	32.4	32.71	27.9	21.3' x	84° 59.6	130
	2104	32.7	33.05	28.1	21.6 x	56.6	110
	2135	32.6	32.88	28.1	22.1 x	53.1	
	2205	32.7	33.12	27.8	22.4 x	50.8	83
	2242	33.5	33.74	28.0	22.8 x	47.2	
	2305	34.1	34.16	27.8	23.1 x	45.0	
	2343	34.2	34.33	27.8	23.6 x	41.4	
6/20	0017	34.1	34.28	27.7	24.0' x	38.1	
	0107	33.9	34.09	27.8	24.7 x	33.3	65
6/20	0136	34.0	34.47	27.8	25.1 x	30.3	72

width

13

amst
Depth. m

Time	Sr	St	T ^o C	Loc.	amst
0205	34.0	34.30	27.6	28°25.7' x 84°27.0'	C1 63
0234	34.0	34.21	27.5	28°26.2' x 84°23.8'	60
0303	34.0	34.24	27.5	28°26.6' x 84°20.4'	60
0404	34.5	34.76	27.6	28°27.5' x 84°15.3'	43
0453	34.9	35.10	27.6	28°28.5' x 84°07.5'	45
0545	34.8	35.36	27.6	28 33.07 84 8.51	42
0700	34.6	34.96	27.6	28 36.66 84 13.65	42
0805	34.2	34.60	27.3	28 35.85 84 20.47	
0955	33.3	33.85	27.6	28 36.46 84 30.1	57
1100	33.7	34.04	27.6	28°40.42' x 84°26.9'	63
1200	34.4	34.64	27.5	28°41.29' x 84°19.35'	43
1300	34.4	34.57	27.5	28°38.14' x 84°15.83'	35
1416	34.4	34.61	27.6	28°30.2' x 84°15.2'	45
1503	34.3	34.61	27.6	28°25.1' x 84°14.8'	
1615	33.9	34.30	27.7	28°21.7' x 84°17.8'	N-1.1 53
1630					N 1.1
1702	34.4	34.45	27.7	28°19.0' x 84°22.4'	NNW 1.52 63
1730					121 km
1809	34.5	34.68	27.7	28°15.3' x 84°28.8'	NNW 1.2 70
1914	34.5	34.91	27.6	28°10.5' x 84°33.4'	NNW 1.2 75 12
2045					1.2 102
WIND SPEED DUE W 20km					
2005	34.4	34.86	27.5	28.07.4' x 37.3'	83
2046	34.7	34.90	27.3	28 05.4 84 40.29	90
2125	33.8 (corr 34.2)	34.01	27.5	28 03.33 84 43.61	95 1.2 22
2200	(32.7)	33.14	27.5	28 00.43 84 46.3	342 1.2 150
2255	32.6	32.97	27.45	28°58.44' 84°50.68	212m
0043	32.7	33.06	27.4	27°51.7' x 84°59.4'	311
0131	33.7	33.73	27.3	27°48.2 x 85°03.3'	364
(25)					

14

Course?
Curren

Time Z	σ_R	σ_S	$T^\circ C$	Loc	depth m
✓ 0207	33.7	33.73	27.3	27° 44.5' x 85° 05.7'	427
✓ 0304	32.8	33.20	27.4	27° 39.2' x 85° 09.9'	534
✓ 0407	33.7	33.61	27.2	27° 33.2' x 85° 14.1'	744
✓ 0502	32.9	33.00	27.5	27° 29.7' x 85° 16.7'	871

Sta 25

✓ 0700	32.5	33.00	27.5	27° 22.27	85 19.77	SURFACE
"	35.8					25m
	35.6					15m
	35.3					8m
	33.2					4m
✓ 0855	33.5	33.27	27.4	27.22.82	85 11.65	816m
✓ 0915 ^{STA} 26	33.5	33.35	27.4	27° 22.34	85° 09.09	766m
✓ 1100 ^{STA} 27	33.5	33.56	27.2	27° 22.1' x 85° 02.5'		525m
✓ 1438 ^{repeat} 25?	34.3	34.58	27.4	27° 21.9' x 85° 20.5'		1109m
1602 ^{STA} 24	35.6	35.62	27.0	27° 22.1' x 85° 30.2'		2700m
2012 2008	35.9	35.89	27.5°	27° 21.2	85 35.6	3245m
✓ 2200	35.2	35.43	27.6	27° 21.29	85 43.65	~3200

1730 8/2

1.2

1800

1831

1.3

1910

1.8

2000

1.3

2031

1.4

2100

1.4

2130

1.3

2210

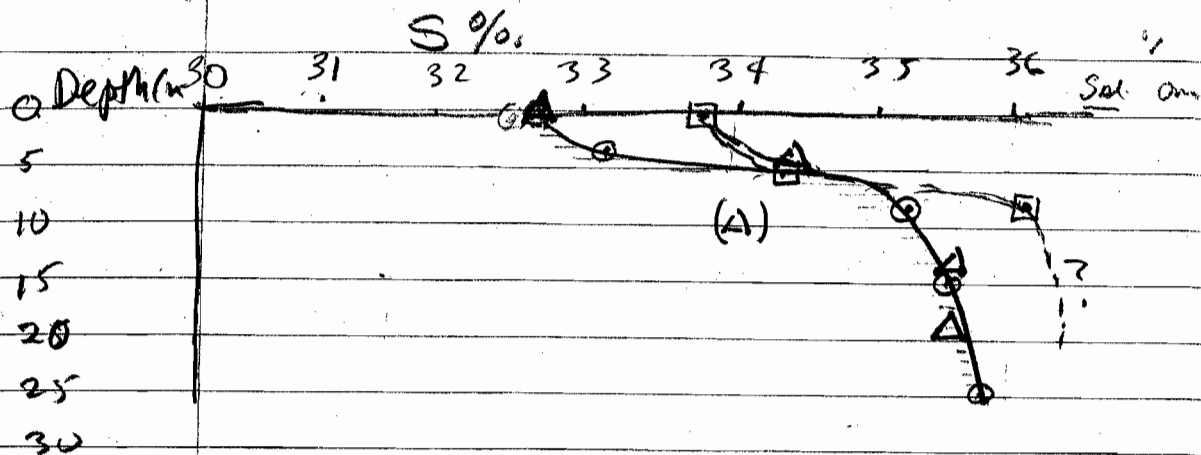
1.1

2230

1.0

⑩ 2300

1.6



15 fcm 275

Depth	CAST	S ‰	m
1	32.5	9.2	.092 m
2	32.5	8.75	.0875
3	32.5	8.2	
4	32.15	8.0	
5	32.5	7.75	
6	32.4	4.5	
7	32.0	2.8	
8	32.1	2.5	
9	32.2	2.2	
10	32.25	1.8	
11	32.3	2.0	
12	32.4	1.7	
13	32.4	1.6	
14	32.5	1.4	
15	32.6	1.1	
16	32.6	1.1	
17	32.65	1.0	
18	32.7	.83	
19	32.7	.82	
20	32.75	.7?	
21	32.8	.6	

68.6 .686 m .686

$$\begin{aligned}
 & 45 \times \frac{90}{4050} \times 1.4050 \text{ m}^2 \times 2.56 = 10368 \text{ cm}^2 \\
 & = 10368 \times 10^6 \text{ m}^2 \times .686 \text{ m} \\
 & 7.05 \times 10^9 \text{ m}^3 \\
 & \approx \text{fresh water R.}
 \end{aligned}$$

16

Time	S _R	S _S	T ^o C	Loc.	Depth m
✓ 0209	35.5	35.80	fauces	27° 21.9' x 86° 00.7'	1333
✓ 0425 ^{STA 22}	35.8	35.88	27.6	27° 21.6' x 86° 15.0'	3190
✓ 0715 ^{STA 21}	35.7	36.02	27.75	27° 21.92 86° 35.64 ^{50°}	3085
✓ 1631 ^{STA 19}	35.2	35.07	27.2	27° 51.4 x 87° 00.15 ^{50°}	2963
✓ 1830	34.2	34.13	27.5	27° 52.8 x 86° 46.3	2948
✓ 1848	34.1	34.25	27.3	27 52 50 86 42 00	2952
✓ 2000	34.4	Cast - 6 m w angle of 20° [5.6] 142.5			
"	36.2	" - 10 m w angle of 40° [7.7]			
" surface STA 18	33.7	34.11	27.9	27° 51.2 x 86° 35.7	3048
✓ 2355 ^{STA 17}	34.0	33.88	27.5	27° 50.6 x 86° 15.2	3170

6/23/80

450 Sta 16 Surf

Heavy rain 32.4 32.75 27.1 27 50.66 86° 00 038 1.0 2925 m

pore w pore 37.0 Sta 16

✓ 0715 SURF	34.0	34.15	27° 50.84 85° 40.90	OK
✓ 0825	34.0	34.19	27 50.73 85° 45.2 km	1093
✓ Sta 15 Pore	34.9	33.32	27 50.73 85	little more
✓ 1345 6/25	32.8	33.32	27° 51.12 85° 24.01 w	
✓ 1415 6/25		33.19	27° 51.03 88° 19.66	500
✓ 1500 ^{STA 13} surface	32.7	33.14	27° 51.1 x 85° 15.9	528

4m - 32.7

7m 34.13

10 34.0?

13 35.4

19 35.3

.1 km

Early 24 2.4m 050 → 050 1 km

28 10m 40 → 320 .4

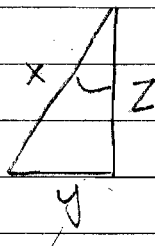
27 3 138 → 318 .4

6/22 0700 GMT 050 → 230 .5

1240 GMT 090 → 270 1.4

1545 138 → 318 .4

2000 192 → 322 .5



$$\cos \theta = \frac{Z}{X}$$

$$X = \frac{Z}{\cos \theta}; Z = X \cos \theta$$

0329 04 6/23

from 038 → 218 1 Knot

Sta 16

SU ↑



1500 - 2000 6.6 km

-1900 tidal current

0160 038-218 .7 Knot

Time	S _R	S _S	T [°] C	Loc	Depth m
✓ 1738	32.5	33.14	28.1	27°50.7' x 85°09.2	
✓ 1805	32.7	33.02	28.2	27°50.7' x 85°06.7	405
✓ 1906	32.6		28.3	27°50.8' x 84°59.4	295
Kant topography 1907 & 1913					
✓ 1944	32.5	32.87	28.4	27°50.8' x 84°54.5'	260
✓ 2025	32.6	32.94	28.6	27°50.7' x 84°49.5	210
2100	32.8	32.92	28.3	27°50.6' x 84°45.4	165
2150	32.7	33.12 Ron	28.4	27°50.9' x 84°39.6	140
2240	33.4	33.62	28.0	27°51.4' x 84°35.2	100
2314	33.0	33.74	28.2	27°51.6' x 84°29.8	75
2335	33.8	33.89	28.3	27°51.35' x 84°27.94	75
6/24 0040	34.0	34.19	28.1	27°50.8' x 84°19.7	75
0122	34.4	34.72	28.5	27°51.1' x 84°14.7	75
0202	34.3	34.64	28.0	27°51.3' x 84°09.8	65m
0251	34.3	34.47	28.1	27°50.9' x 84°03.8	60m
⑦ 0327	34.4		28.0	27°50.6' x 83°59.4	50m

18

Rm Museum

Time	S_R	S_S	$T^{\circ}C$	Loc.	Depth
0454	35.3	35.35	27.6	27°50.7' x 83°49.6'	85m
0400					021 1.3
0430					021 1.5
0500					034 1.4
0515					050 1.6
0530					
		can 30m			
0715	34.6			27°51.04' 83°35.24'	36m
0530					075 1.0
0600					066 1.1
0630					066 1.1
0700					069 1.2
0730					098 1.6
0800					098 1.6
0620	34.6	34.92	28.0	27°50.26' 83°40.76'	
0715	34.6			27°51.03' 83°35.24'	
0745	35.0	35.27		27°51.06' 83°32.18'	
0		35.69			
0905	35.5	32.97	27.3	27°51.08' 83°28.6'	
0830					100° 1.5
0850					071 1.3

25 June 80

Drill core to be tested with divers.
10 foot core - max. is 25'.

Drill Station #1
32' depth

27°50.96' x 83°02.05'

Surface sample taken by divers → +++ P test

Surf Sand, shelly quartz sand
with qtz $\frac{1}{16}$ - $\frac{1}{2}$
shell & benthic forams
white & black ~ 1mm

~~Brick~~ ~~fine~~ coarse
Coarse $\frac{1}{2}$ #
med. $\frac{1}{25}$ - $\frac{1}{12}$
fine sand $\frac{1}{16}$ - $\frac{1}{8}$ (f)
silt. $\frac{1}{16}$ - $\frac{1}{256}$

[Note: top of core - muddy sed. is in part eroded from core]



Archaeus angulatus - reefal form?

Peneroplis proteus? Bahama



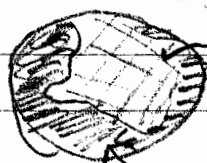
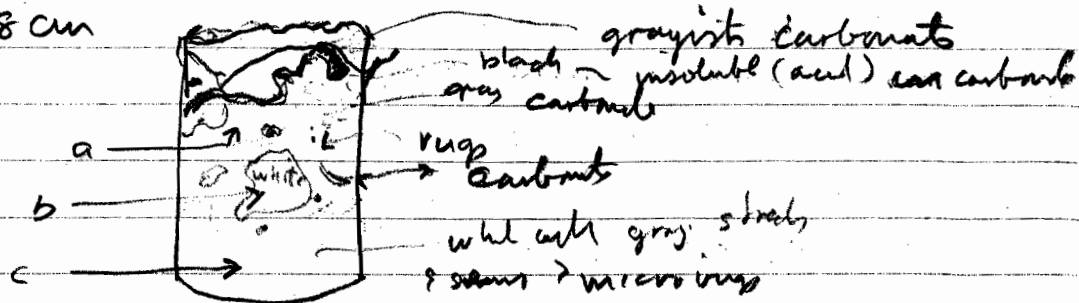
banded
gray dolomite

- Green - buff, calcareous cemented grain, yellowish
put. of grain - 1.0 x .3 P very sand
- Peneroplis - proteus .6 black P-
- Vitreous phosphatic grain 1. x m P very sand
aggregated 15 μ particles amber - brown - buff
- Brach. rounded spined (microchale) aggregate P
~~1mm x 5 x 3 mm~~ with sand
round ~ organic (form) casts .03 mm
- gray Peneroplis frag and with P-
pores open
- amber calcareous grain black gutules Pt Pt
- gray white griddle, white yell & green .25

H. Reicheni peneophras grain? P - very faint?
pores?

i Coral grain 2 mm P-

3-8 cm




Test on black material, possibly pyrite minerals

Surface black & phosphate coated
black-gray carbonate, with white
streaked carbonate below;

- a. High rugula crystalline limestone P+
with quartz grains (fine sand), 1 grainy
medium fine-mid sand size phosphate run
! some bull dolomite frags
- b. ~~some~~ white pure carbonate
- c) same as a)

8-14 cm white cemented ls
with darker grains P+
bottom & top
few quartz grains

15-20 white speckled limestone, heavily
microcrinulid with .1-5 mm cavities
Very highly rounded quartz grains
& phosphatic grains P+
Cream-colored veins of regular carbonate
with no quartz P+

20-23 Hard buff speckled ^{microcrinulid} phosphatic
limestone; top with rounded
qtz grains; bottom subrounded
Frequent arcuate cavities; 
Sand fine grained, as above. 1 bladed rug

23-25 As above, revised;
Rugs are commonly chevroned channels
not molds of organisms

28-33 As above

33-36/aa 3 mm rug with bladed
wall



36-39 aa

40-43 Buff, ^{sparingly} sugary, microcrystalline
dolomite ~~benzene~~ with occasional phosphatic
~~speckles~~ ~~and~~ speckles (rounded
grains much denser than
previous samples; Strong phosphate reaction

44-50 Very hard buff dolomite, sugary
sparingly microcrystalline, with speckles of phosphate

50-51 aa buff-speckled

50-54 Hard microcrystalline sugary dolomite
with fine-very fine quartz sand and
phosphatic inclusions P+

54-58 aa

58-61 aa

Total core 61 cm

26 June 80 - Drill Site #2

Seas too high to try drilling.

Frank has had Theo make a dart core out of pipe ~ 2½ feet long. Will try to punch a hole in strata @ drill site.

GC-2 "Dart Core" 27°49.70 Drill Core S. In 2
 1450 83° 33' 00" Core 1 Sanded
 Brown, fine silty-clayey foraminiferal mud with glauconitic streaks Core 2 3" of brown - gray plastic silty sediment P-

Sample Smith McIntire #1 27°51. P-
 SM-3 whole sample 83° 28' green fine
 Green gray highly calcareous, fine grained sand, light glauconitic sandy sed.

Sample Smith McIntire #2 27°50.44 silty
 SM-4 Green gray silty, ov. fine carbonate sand, minor qtz 83° 27.84
 abundant qc grains
 In fact 18 cm brownish sand graduated
 dolomitic to heavy clayey sand.
 dark grains
 one with PT

Samples 0-2 cm - P Green fine silty sd with qtz
 2-5 cm - P V. fine silty carb. sand with qtz & large qc inclusions
 5-8 cm - P - ref. silty carb. sand
 P-12 cm - P with dark stained carb. grains
 12-18 cm - P PA

Sample

Drill Site #2 - Smith - MacIntyre #3

29° 50.83 x 83° 31.25

SM-5

Dark gray - speckled sand, w/ black specks
stained carbonate, many benthic forams

Samples:

some glauconite, scarce

0-25 cm -

P -

Bottom -

P -

Summary

25

Piston Core Locations + Tests

	STA.	Pore W. Sp.	Loc.	Cl %	P	Length ft.
6/18	3	34.8	28°18' x 87°01'	19.5	-	22.5
"	4	34.7	28°18' x 86°49'	19.5	-	32
"	5	35.0	28°18' x 86°36'	19.5	-	32
"	7	35.1	28°18' x 86°12'	19.7	-	32
6/19	8	35.3	28°18' x 86°00'	19.5	-	21
"	9	35.5	28°18' x 85°47'	19.8	-	32
	24	35.4	27°22' x 85°30'	19.6	-	30
	26	35.4	27°22' x 85°09'	19.8	-	31
	27	35.4	27°22' x 85°02'	19.6	+	32 (Top 2' kept)
	23	36.0	27°22' x 85°45'	20.5	-	20
	22	35.8	" x 85°15'	19.7	-	22
	21	36.3	27°21.4' x 86°36'	19.46	-	31
	20	37.0	27°22' x 86°60'	19.8	-	30
	19	34.3	27°51' x 86°00'	19.6	-	30
	18	32.3	" x 86°36'	19.3	-	24
	17	36.7?	" x 86°15'	22.1	-	26
	16	37.0	27°50.4' x 86°00'	20.7	-	16
	15	34.9	27°51' x 85°46'	19.5	-	29
J	14	35.3	" x 85°31'	19.8	-	35
J	13	35.5	" x 85°16'	19.7	-	25
	1	35.2	28°59.8' x 88°05.4'			29
	2					

26

27 June 80

Water data en-route June 26

GMT	S _s	Loc.	T°C	S _a	Depth
0403	34.08	26° 45.28 84° 04.30	28.1	Ref 33.9	
0615	33.38	26° 24.83 84 11.45	28.3	Ref 32.9	170
0715	33.95	26° 16.10 84 15.79	28.2	Ref 33.6	183
0910	35.34	26° 00.02' 84° 23.85	28.5	35.0?	213 m
1010	35.43	25° 59.96' 84° 17.18'	28.3	32.5?	190m
1120	33.58	25° 59.97' 84° 10.19'	28.2	33.6	190m
1630	34.62	26° 00.02 83° 38.44	29.3	34.3	
1750	34.91	26 00.06 83 33.66	29.5	34.8	75m
1840	34.68	26 59.96 83 28.08	29.6	34.6	68m
SURFACE WATER		34.839 S 700		34.0	
2000	34.39	25° 59.7 83 13.9	29.5	34.2	66
2200	34.98	25° 59.97 83 00.30	29.2	34.4	52
2300	36.01	26° 00.03 82° 55.34	29.3	35.8	40m

27 June 1980

Bomb grab sample (U.S. I. Underway Sampler)
 Surface

Fine grain sand + silt w sea weeds

26° 00.03' x 82° 55.34'

43 meter

P -

2348 GMT 36.23 26° 00.07 x 82° 49.72' 29.2 36.0 43m

28 June 80

Time	δ_A	δ_S	$T^{\circ}C$	Loc.	Depth. M
0027	36.0	36.18	29.1	$26^{\circ}00.02' \times 82^{\circ}44.89'$	40

Bomb
Grab

U.S. #2 32 m 0100 6/28
 $26^{\circ}59.96' \times 82^{\circ}40.90'$
 P -

0125	36.2	36.40	29.2	$26^{\circ}00.0' \times 82^{\circ}38.12'$ ^{end of line 11}	30
0230	36.1	36.27	29.0	$25^{\circ}53.35' \times 82^{\circ}37.91'$	42 m
0415	35.8	36.00	28.8	$25^{\circ}50.02' \times 82^{\circ}46.38'$	46 m
0520	36.0	36.14	29.0	$25^{\circ}49.95' \times 83^{\circ}53.51'$	52 m
0640	35.4	35.79	29.0	$25^{\circ}50.40' \times 83^{\circ}3.17'$	56 m
0825	35.0	35.05	28.8	$25^{\circ}50.03' \times 83^{\circ}15.78'$	65 m
0940	34.2	34.52	29.3	$25^{\circ}49.99' \times 83^{\circ}24.93'$	71 m
1050	34.7	35.21	29.2	$25^{\circ}50.07' \times 83^{\circ}32.23'$	78 m
1140	34.4?	35.00	29.1	$25^{\circ}49.90' \times 83^{\circ}57.65'$	76 m
1313	32.8?	34.68	29.1	$25^{\circ}50.12' \times 83^{\circ}46.18'$	90 m
1405	33.9	34.16	28.8	$25^{\circ}49.98' \times 83^{\circ}49.77'$	115 m
1456	33.7	33.91	28.9	$25^{\circ}49.90' \times 83^{\circ}55.41'$	127 m
1542	33.7	33.71	29.3	$25^{\circ}49.87' \times 84^{\circ}00.75'$	140 m
1621	33.6	33.63	29.1	$25^{\circ}50.04' \times 84^{\circ}05.32'$	145 m
1702	34.6	34.69	29.5	$25^{\circ}49.85' \times 84^{\circ}10.23'$	157
1755	35.9?	35.38	29.7	$25^{\circ}49.98' \times 84^{\circ}15.28'$	160
1847	35.5	35.48	29.6	$25^{\circ}50.15' \times 84^{\circ}21.08'$	188
1920	35.3	35.45	29.6	$25^{\circ}50.18' \times 84^{\circ}25.22'$	208
1958	35.4	35.65	29.8	$25^{\circ}49.98' \times 84^{\circ}30.09'$	227
2039	35.8	35.95	30.1	$25^{\circ}50.05' \times 84^{\circ}35.26'$	377

U.S. Bomb Grabs

U.S. #3 Course gray-brown sand w black + white inclusion 0500 6/28 25°50.39' x 82°38.04'
P -

#4 Fine grain gray-green sand + silt 25°49.98' x 82°52.01' 50m
P -

#5 Course grain brown-gray sand with some silt and large white + black inclusions 25°50.44' x 83°05.30'
P -

#6 very small sample - not representative

#7 Medium grain brown sand with some very fine brown sand with small black inclusions. contains large shell and coral fragments. 25°50.1' x 83°33.8' - 80m
P -

#8 - No Sample

#9 + 10, 11 - No Sample - too deep

#11 29 June 50 1055-E 25°40.03' N x 83°36.12' W 82 metres - Fine grain green-gray sand and silt, small white shell fragments, few dark species.

#12 25°40.4' x 83°18.2' 62m P -

Course shell + coral fine silt - *Religia cretacea* type weather swimming animal P -

see p. 31 for cont.

28 June Speed & current

0400 - 0430 036 → 216 .9k3-
 530 - 0600 0 01kn4-
 700 - 730 110 - 290 1.1.5
 0730 - 800 030 - 210 .9

Waters

Time	S _R	S _S	T°C	Loc	Depth-m
2122 ²⁸ June	35.2?	35.76	30.2	25°50.10' x 84°40.62	746
2203	34.5	35.41	30.0	25°50.01' x 84°45.99	1163
2330 ²⁸ June 13	35.3	35.42	29.7	25°50.12' 84°57.06	3329

Currents 2200 - 2330 107 - 1.4 knot

29 June 80

0121	35.6	35.60	28.7	25°39.95' x 84°57.98	3343m
0232	35.3	35.32	29.2	25°40.06' x 84°49.16	1500
0306	35.2	35.36	29.2	25°40.04' x 84°44.74	1200
0338	35.3	35.32	29.1	25°39.99' x 84°40.09	950m
0408	35.6	35.69	29.2	25°40.08' x 84°35.70	619m
0520	35.8	36.07	29.2	25°40.10' 84°25.79	225m
0645	34.7	34.98	29.3	25°40.18' 84°12.42	170m
0730	33.7?	35.65	28.8	25°40.0' 84°05.53	149

June 28 1700 320 → 140 .8 knot

1830 010 → 190 .6 knot

currents & directions

June 29

0430 170 → 350 .3k 0600 190 - 010 .6

0500 180 360 .4 0630 175 - 855 .6

0830 180 - 360 .5k 0700 210 - 030 .8

0730 240 → 060 .8

Time	Refr %00	Sal ‰	T °C	Loc	Depth
0835	33.8	33.95	29.1	25° 40.15' x 83° 56.43	136 m
0918	34.2 ?	34.69	29.2	25° 40.33' x 83° 49.78	115
0950	35.0	34.98	29.5	25° 40.20' x 83° 45.45	103
1025	35.0	34.94	29.5	25° 39.97' x 83° 38.22	87
1118	34.4	34.54	29.4	25° 40.00' x 83° 33.47	78
1147	34.4	34.52	29.4	25° 39.93' x 83° 28.95	74
1248	34.6 ?	34.96	29.6	25° 39.97' x 83° 19.26	67
1354	35.3	35.25	29.5	25° 39.97' x 83° 10.07	54
1513	35.7	35.83	29.6	25° 40.06' x 82° 59.70	47
1652 ^{and 15}	34.8	35.13	29.4	25° 38.96' x 82° 49.10	41

Currents

Local Time

0400-0430	228.6'	.8	29.7 Time
430-0500	210.5	.8	Time
500-0530	232.2	.5	Time
0530-0600	221.2	0.5	Time
0600-0630	222.0	0.7	Time

plotted

1822	35.2	35.34	30.3°	25° 29.98' x 82° 50.71	43 m
1944	35.0	35.29	31.1°	25° 30.41' x 83° 01.35	50 m
2045	34.5	34.72	30.8°	25° 30.06' x 83° 08.87	54 m
2145	34.5	34.75	30.4	25° 30.04' x 83° 17.37	59
2330	34.6	34.79	30.7	25° 30.07' x 83° 30.22	68
30 June 0057	34.2 ?	34.49	29.9	25° 29.90' x 83° 41.93	82
0158	33.9	34.49	29.9	25 29.82' x 83 50.98	108
0318	33.6	33.67	29.7	25 29.60' x 84 01.43	137
0430	34.7	34.76	29.7	25 29.50' x 84 10.42	164

U.S. Bomb Grabs (cont)

#13 Gray-greenish med-fine sand, many black specks with a few white fragments.
 $25^{\circ}39.95' \times 83^{\circ}05.65'$ depth 60m
 P -

#14 $25^{\circ}39.88' \times 82^{\circ}52.15'$ depth 43m
 Fine-med greenish-gray sand w small black specks.
 P -

Current local time June 29

20	1600	125-305 .7	plotted
20 ⁰⁰	1630	100 - 280 1.2	
21	1700	160 - 340 1.3	
21 ³⁰	1730	170 - 235 1.4	
22	1800	185 - 345 1.6	
	1830	getting current N 1km	
23	-1900		

steer made
 2030 - 2200 271 269.3 7.5

Line 1 $183^{\circ}45'$ sudden current
 current to N

speedometer

Pitot-static tube bottom of hull

32

<u>Time</u>	<u>Spref</u>	<u>S_{sat}</u>	<u>T_c</u>	<u>Loc</u>	<u>Depth</u>
G830/80					
0540	34.3	34.63	29.5	25°29.80 84°20.36	157 m
0640	35.16	35.66	29.3	25°30.08 84°28.36	366

Bridge

Lat-Long only correct near good

GMF

2340 - 0200	069 - 249	.5	<u>June 30</u>		
0200 - 0330	057 - 237	.6			
0430	022 - 202	.5			
0500	090 - 220	.3			
0530	124 - 304	.2			
0600	177 - 003	.4	irregular		
0630	100 - 288	.4			
0700	090 - 270	.2			

0800	35.0	35.5	29.0	25°30.02 84°39.13	
1438	34.2	34.48	29.4	25°18.05 x 84°19.71	
1549	33.8	34.13	29.1	25°17.81 x 84°09.92	
0925 nd line	35.3	35.47	28.7	25°27.88 x 84°47.61	2000 m
1035	35.0	35.22	28.5	25°20.92 x 84°46.83	~3000 m
1707	33.7	34.17	29.4	25°17.23 x 83°58.95	128 m
1825	34.3	34.48	29.6	25°17.77 x 83°48.43	105 m
1932	35.2	35.11	29.7	18.05 39.59	75 m
2157	35.1	35.30	29.3	25°17.97 x 83°20.86	62
2323	35.3	35.51	29.7	25°18.10 x 83°10.16	57

(12)

1 July 80

Time	S _R	S _S	T [°] C	Loc	Depth m
0007 ^{end} line 19	35.0	35.19	29.2	25° 17.80 x 83° 04.97	55 m
0153	35.4	35.29	29.6	25° 10.00 x 83° 10.66	57 m
7/1/80					
0430	34.3	34.73	29.2	25° 09.96 x 83° 30.70	69 m
0605	34.3	34.83	29.2	25° 09.88 x 83° 41.92	82 m
0730	33.8	34.00	29.0	25° 09.91 x 83° 52.79	115 m
0919	35.5	35.66	28.7	25° 08.52 x 84° 45.29	~3400 m
1537 ^{line} 23	35.4	35.59	28.6	24° 59.98 x 84° 40.20	3375 m
1710	35.2	35.49	29.2	24° 59.95 x 84° 27.96	1875
2010	34.0	34.26	29.4	25° 00.06 x 84° 04.75	190
0840	33.6	33.80	28.8	09.52 02.59	140

CURRENT INFORMATION

000 0400-0430	298.6°	0.8 KNOTS
030 0430-0500	210.5°	0.8 "
060 0500-0530	232.2°	0.5 "
090 0530-0600	221.2°	0.5 "
000 0600-0630	222.0°	0.7 "

1005	34.1	34.34	28.9	25° 10.01 ^{84°} 12.79	160
1107	34.0	34.37	29.1	25° 10.00 ^{84°} 21.09	410
2237		34.43	29.5	24° 50.54 x 83° 10.31	390
0950 July 2	34.28	28.6		24° 50.29 x 83° 50.89	75
1046	34.63	28.7		24° 45.97 x 83° 53.75	186
1148	34.65	28.7		24° 41.30 x 83° 58.90	900
July 3 0510	35.3	35.61	29.2	25° 00.01 x 83° 04.67	52

7/1

TIME

Plotted in table

LOCAL	GMT	COURSE STEERED	SPEED BY ENGINE	COURSE MADE GOOD	SPEED MADE GOOD	SET FROM/TO	DRIFT
0000	0400	270	7.2	269	6.8	$\frac{286}{106}$.4
0030	0430	270	7.2	270	6.8	$\frac{270}{90}$.4
0100	0500	270	7.2	270	6.6	$\frac{270}{90}$.6
0130	0530	270	7.2	270	6.6	$\frac{270}{90}$.6
0200	0600	270	7.2	268	7.0	$\frac{320}{140}$.3
0230	0630	269	7.2	266	7.2	$\frac{357}{177}$.4
0300	0700	274	7.2	268	6.8	$\frac{332}{152}$.8
0330	0730	282	7.2	274	7.4	$\frac{019}{199}$	1.0

U.S. Bomb Grabs (cont)

#15 $25^{\circ}29.95' \times 82^{\circ}52.03$ 52m

Fine gray-green sand with small black specks - very homogenous
P -

#16 Medium-fine gray-green sand with white & black specks - some large shell fragments $25^{\circ}29.82 \times 83^{\circ}05.28$ 75m
P -

#17 Mixed greenish brown fine sand with ground shell hash. $25^{\circ}30.03 \times 83^{\circ}17.80$ 58m
P -

#18 Light brown ^{fine} shell hash. $25^{\circ}29.97 \times 83^{\circ}36.44$ 71m
P -

#19 Light brown (tan) medium shell hash with small amount of fine silt. $25^{\circ}18.12 \times 83^{\circ}36.42$ 70m
P poss. trace

#20 Grayish-brown shell hash with medium-fine sand. $25^{\circ}18.3' \times 83^{\circ}18.3'$ 60m
P poss. trace

#21 Medium shell hash with gray-greenish sand, many black specks. $25^{\circ}18' \times 83^{\circ}06'$ 53m
P -

#22 medium - fine gray-green sand with
black specks & few large shell

$25^{\circ} 10.59' N \times 83^{\circ} 05.65' W$ 70 m

P - green reaction w/ ^{isolated} black specks

#23 $25^{\circ} 10.05' N \times 83^{\circ} 18.21' W$ 55 m

medium - fine shell hash w/ small amount of
fine sand (echinoderm extremity - brittle star?)

P -

#24 mixture of medium - fine shell hash and fine
light brown (tan) sand. [chunks of red coral].

$25^{\circ} 10.03' N \times 83^{\circ} 36.85' W$ 70 m

P -

CONCEPT OF CALIBRATION CURVE, TITRATIONS \rightarrow SALINITY

$S_v = \text{wt/vol. units (g/l)}$ $d = \text{density at oper. temperature}$

$S_w = \text{wt/wt units (g/kg)} = \text{Salinity}$ } We can measure only volume

$$\frac{S_v}{S_w} = d$$

$$S = 1.806 \times \text{Cl } \%$$

To obtain approximate direct calibration curve choose fresher water and standard sea water determine S salinimetrically (Bissett Berman) and by titration. Plot on suitable graph.

Although points should be slightly curved a straight line for small differences will be approximately correct. ~~the~~ We must further assume that relationship S/Cl is constant. This will hold for ~~surface~~ Ocean waters but not necessarily for pore waters. These should be checked at lab if possible.

Further if we wish to run higher samples than curve (straight line) allows we may run them salinimetrically and by titration to extend curve. High sal. may be obtained by evaporating sea water.

LINE 1 Delta - $88^{\circ}44'$, on 29°

LINE 2 N $88^{\circ}44'$ to $30^{\circ}09'$

LINE 3 FROM LINE 2 to $29^{\circ}00'$ $88^{\circ}07.8'$ Core 1

LINE 4 FROM CORE 1 to $87^{\circ}37.5'$, $30^{\circ}07'$

S. of Mobile Bay

Line 5 From 4 to Core 2 at $87^{\circ}37.5'$, 29.00

MANHEIM LINE FROM Core 2 to

TARGET $84^{\circ}10'$
24 51.9

2nd leg 83.34
24 46

2 July 1980

Dredge line #1

		<u>Time</u>	<u>Loc.</u>	<u>Depth</u>
Haul #1	over board	0107Z	24° 48.26' x 84° 12.49'	850
	on bottom	0124Z	24° 48.16' x 84° 12.23'	875
	off bottom	0155Z	24° 48.20' x 84° 11.73'	875
	on board			

Superficial Gray brown - very fine sediment (clayey) with lumps of clay. Few organisms, one coral-like structure.

Paleo work Sand ~ 30%, many many siliceous particles (specimens etc.)

P sediment -

P clay -

Paleo - tentative Pleistocene → recent

Line #1

haul #2

On bottom $24^{\circ} 49.31' \times 84^{\circ} 11.71'$ 530m

Off bottom $24^{\circ} 55.84' \times 84^{\circ} 11.67'$ 460m

- incorrect

Grayish-green sandy sediment

Exclusions - brittle stars, few shell, "kinker"

Paleo wash - carboniferous + siliceous tests
and spicules

P sed. -

Paleo - Pleistocene to recent.

Dredge line #1 - Haul #3

	<u>loc.</u>	<u>depth</u>
On bottom	$24^{\circ}54.63 \times 84^{\circ}05.21$	212 m
Off bottom	$24^{\circ}55.00 \times 84^{\circ}04.70$	180 m

Lost dredge @ surface - cross bar broken.

~~are~~ Rocks in dredge appear to be globular, tan phosphorite?

↑ NO →

Line #1 - Haul #4

New Dredge (claw type clam dredge)

On bottom $24^{\circ}54.51' \times 84^{\circ}05.51'$ 220 meters
 Off bottom $24^{\circ}51.77' \times 84^{\circ}04.25'$ 205 meters

Algal Reef Rocks - ^{Carbonate} Rubble

Separated into categories:

- ① New Material
- ② Nodular
- ③ Worn Nodular
- ④ Weathered
- ⑤ Organic Stained

P -

Paleo Pliocene → recent forams

Line #1 - Haul #5

On Bottom: $24^{\circ} 54.90' \times 84^{\circ} 04.80$ 205mOff Bottom: $24^{\circ} 55.10 \times 84^{\circ} 04.65$ 178m

Carbonate algal Reef material
 "rocks" + 2 plate forms.
 Representative collection made.

P small plate: black stain ~ +
 brown stain ~ +

shells?

or Fe oxide ppt.

A nodule: black stain -
 brown stain -

Paleo Pleistocene \rightarrow recent

Line #2 - Haul #1

On bottom . 41.30 59.26

Off bottom 24° 41.42 x 83° 59.33 735

2000 lb. pull 24° 41.42 x 83° 59.28 787.5 meter

Greenish-gray clay -

Nudge Wash - shell hash with a few organisms

P sed -

Line #2 - Haul #2

On bottom	24° 41.98 x 83° 59.10	625m
Off bottom	24° 42.25 x 83° 59.01	546

Tug @ 24° 42.26 x 83° 58.99

Greenish-gray sandy shell hash

Large piece of brown coral (Tubular)

Piece of Fresh sheared carbonate outcrop

Paleo - weather side of carbonate - brachiopods

P sediment ~ ~ +

P clean shear $\frac{1}{2}$ +

P black + brown staining -

P brachiopod shell -

Paleo Calcified worm tubes, agglutinated annelid tubes with mm-sized material (sponge spicules, forams, grains - obviously a sampling of sediment at bottom) Coral surface seems recently dead, not heavily bored nor over 50% covered with epibionts. Coral fragment not greatly abraded & rounded - not transported very far. [Descriptions of Coral Fragment - Scott Brander]

Dredge Line #2 - Haul #3

On bottom	$24^{\circ}42.68' \times 83^{\circ}57.45'$	463 meters
Off bottom	$24^{\circ}42.79' \times 83^{\circ}57.38'$	460 meters

Tugs @ .92 .27 420 meters

hung up on bottom @ raising

Dredge mangled beyond repair!

Few pieces of sheared carbonate material
shells & organisms.

P	fresh sheared pebble	$\frac{1}{2} +$
P	stain pebble (nodules)	$\sim \sim +$
P	brown surface	$\sim \sim +$
P	black surface	$\sim \sim +$

3 July 80
Tortugas Drill site #1

$24^{\circ} 40.35' \times 83^{\circ} 05.00'$

Drill to be deployed in 17 meters of water
with divers and video camera equipment.

Current .3 kt $217^{\circ} \rightarrow 53'$

Camera housing leaked.

Drill bit plugged - not enough water
pressure - No Core.

Fla time June 30

0000	Cstr	Sp	CMG	SMG	Set	Drift
0030	272	7.0	268	7.2	$\frac{022}{202}$.5
0100	272	7.0	270	7.2	$\frac{040}{220}$.3
0130	272	7.0	273	7.2	$\frac{124}{304}$.2
0200	272	7.0	275	7.0	$\frac{177}{203}$.4
0230	270	7.0	271	7.4	$\frac{108}{288}$.4
0300	270	7.0	270	7.2	$\frac{090}{270}$.2
0330	269	7.0	268	7.2	$\frac{050}{236}$.2
0400						

July 3 1980

	LOCAL	GMT	COURSE STEERED	SPEED BY ENGINE	COURSE MADE GOOD	SPEED MADE GOOD	SET FROM/TO	DRIFT
25° 00.1 83° 12.23	0000	0400	101	6.6	090	5.8	151 331	1.4
25° 83° 8.91	0030	0430	098	6.6	090	6	149 329	1.1
25° 83° 05.67	0100	0500	098	6.6	090	6	149 329	1.1
24° 58.2 83° 4.88	0130	0530	182	6.6	183	5.8	174 354	.8
24° 55.6 83° 4.75	0200	0600	178	6.6	177	5.2	181 001	1.4
24° 83° 4.6	0230	0630	180	7.0	177	6.0	197 017	1.1
24° 49.2 83° 4.55	0300	0700	181	7.25	178	6.8	218 038	.6
24° 46.0 83° 4.81	0330	0730	186	6.9	184	6.4	210 030	.6

3 July Time	S_p	S_s	$T^{\circ}C$	Loc.	Depth m
0800	36.0	36.15	29.3	$24^{\circ}42.78' \times 83^{\circ}04.76'$	50
1002	34.4	34.83	29.1	$24^{\circ}30.37' \times 83^{\circ}04.71'$	40
1128	34.4	34.81	29.2	$24^{\circ}20.09' \times 83^{\circ}04.52'$	290
July 4 0055	34.5	34.94	29.5	$24^{\circ}24.47' \times 82^{\circ}59.56'$	100m
0225	34.4	34.66	28.4	$24^{\circ}21.60' \times 83^{\circ}08.52'$	58m
0600	34.2	34.53	29.2	$24^{\circ}30.32' \times 83^{\circ}29.88'$	245m
0645	34.3	34.73	29.0	$24^{\circ}34.97' \times 83^{\circ}23.70'$	60
0730	34.2	34.51	29.3	$24^{\circ}39.63' \times 83^{\circ}25.75'$	60
0830	34.2	34.60	29.2	$24^{\circ}45.81' \times 83^{\circ}23.97'$	64m
1005	34.7	35.00	29.2	$24^{\circ}41.97' \times 83^{\circ}16.15'$	60
1144	35.0	35.15	29.3	$24^{\circ}35.71' \times 83^{\circ}06.38'$	36
1430	35.2	35.30	28.9	$24^{\circ}25.11' \times 82^{\circ}51.85'$	53

TIME

July 4, 1980

LOCAL	GMT	COURSE STEERED	SPEED ENGINE	COURSE MADE GOOD	SPEED MADE GOOD	SET FROM/TO	DRIFT
0000	0400	287	7.25	286	6.4	294 114	.9
0030	0430	293	7.25	291	6.6	312 132	.7
0100	0500	292	7.25	289	6.0	306 126	1.3
0130	0530	293	7.25	291	6.6	312 132	.7
0200	0600	Various		Undetermined			
0230	0630	022	7.25	024	6.8	356 176	.5
0300	0700	021	7.25	022	6.8	006 186	.5
0330	0730	021	7.25	019	6.6	049 220	.7

83 18.94
~~24 24.32~~
~~24 22.19~~
82 56.66
24 25.47
82 22.66
24 26.57
83 22.66
24 27.89
83 28.62

24 33.49
83 28.42
24 36.80
83 27.03
24 39.60
83 25.76

Rick Wall

Paul Schmitt

John Smith

Randy Smith

Scott Brown

Wayne Smith

Tommy Gayton AB's

Jeff Jackson

Larry Tomlinson

Dick Gilson

1852

35.5

24 13.3

6m7

7/7/86

81 44.0

1004

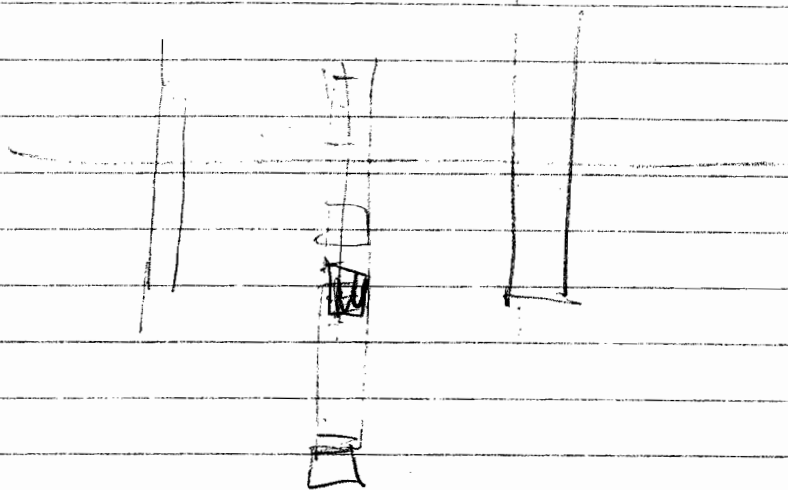
35.1

24 30.42

7/5/80 GMT

80 44.83

0352



TASKS

BRING UP SALINITIES
GET LINE DESIGNATIONS } TIMES FOR
TRANSECTS FOR ACOUSTICS

At Wood Hole

Re do chlorides on pore water \rightarrow Chloridomels

Report to Larry Doyle

Order bottles for Theo

Pick up samples on Gyre - Aug.

- ① Sediments 2 boxes in Fan Tail Frig.
- ② Dredges - Lounge
- ③ Box - Lounge

From
Frank

- Copy of Report
- Select Quotes of Theo Davis

\rightarrow Sign any cruise forms \leftarrow

- 26 cores
- 200 bucket surface water - salinity
 - 22 pore water extractions (piston cores)
 - 5 box cores - 19 samples + description
 - 5 Smith-MacIntyre Grabbs - 1 sample + descrip.
 - 24 Under Way Sample - 24 " "
 - 8 Dredge hauls - 13 " "
 - 106 ~~88~~ Phosphate indication tests
 - ~~88~~ Cl^- titrations
 - 12 Mini hydro Cuts
 - 2 Drill cores - 15 samples + descriptions

3507.7 Km Total (3.5) (~2100 mi)

3292.0 Km Mini Spark

70 sample sites

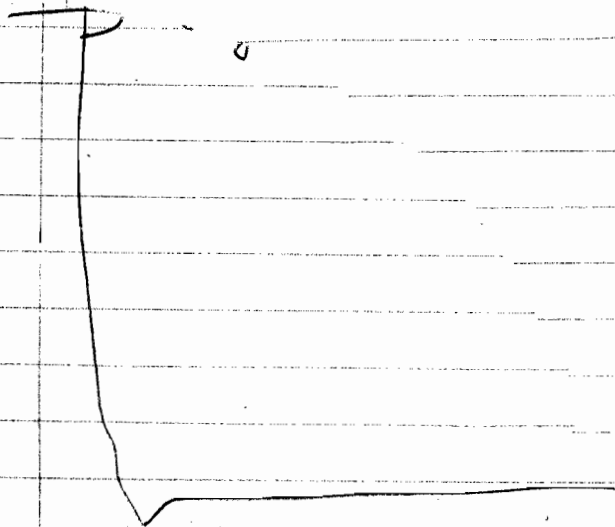
Course plotted + recorded every 15 min.

~~Spencer~~

① 3.5 KH
Recorder

② 800 joule 8 min. spark

The 100 - Michael Hart



Dick

Time Depth Loc Note Age?

① 2133 421

U. M10?

45
16
27.0

②

2140
2138

200m

24 54.75 84 05.12

24 35.66 84 04.01

Pre drill target

M. M10

44

12

56

16

33.6

2135
2142.5

③ 2152, 55

24 51.55
54 05.40

New Start pt

54.78 N

84 05.4

③

③

54.8

84 51.5

④ 2213

oligo?

⑤ 2223

⑥ 2234

Pinnacle
L. Crest Reef?

⑦ 2235

2240
2245

24 49.69

84 11.33

24 49.27

84 11.84

49.42

11.88

51

7 42

62

7

7

22

357

22

42

⑧

2242 - 3.5

505 515

LC.

Braydon 10.27

off bottom 10.32

1051 440

hit ~ 10:32 515

⑧

2248

850

LC.

922 HIT 926 Perched up to 2 1/2 ft.

930 home to 940 off bottom 830m

Shakespeare in context
Museum Pass in Paris

Before we get to the museum
York file me - on the
smaller ones with you

Dredge Sta 2

Bottom N52 214-208m

Fishes about 112

84.05

19.376 / 100 Cl⁻

23 June

Cl⁻

0.5 ml sample

4/100 AgNO₃

Blk. 0.003 ml

Cl mean

STD. 0.003 - 0.841 = 0.838

STA 0.841 - 1.781 = 0.940 } 8 manual pipet must be 1.6

STD. 0.000 - 0.836 = 0.836

STD 0.836 - 1.675 = 0.839

Pore waters

STD. 0.000 - 0.836 = 0.836

STA. 1 0.836 - 1.696 = 0.860

" 0.000 - 0.828 = 0.828

STA. 2 0.828 - 1.666 = 0.838

" 0.000 - 0.838 = 0.838

STD. 0.860 - 1.700 = 0.840

STA. 3 0.000 - 0.836 = 0.836

STA. 3 0.850 - 1.696 = 0.846

STA. 4 0.000 - 0.842 = 0.842

STA. 4 0.860 - 1.702 = 0.842

STD. 0.000 - 0.833 = 0.833

STA. 5 0.850 - 1.693 = 0.843

STA. 5 0.000 - 0.839 = 0.839

STA. 7 0.860 - 1.719 = 0.859

STA. 7 0.000 - 0.850 = 0.850

STD. 0.870 - 1.706 = 0.836

STA. 8 0.000 - 0.841 = 0.841

" 0.860 - 1.702 = 0.842

STA. 9 0.000 - 0.854 = 0.854

" 0.870 - 1.732 = 0.862

STD. 0.000 - 0.834 = 0.834

STA 13

SURF

0.769

19.376

33.14 = 18.35

$$S = 1.806 \times Cl$$

$$Cl = \frac{S}{1.806}$$

$$5/3 = 1.666$$

STD: TAPSO 19.376/100

Doyle
Core catcher

Cl

29 June 80

Sample ^{STD.} 0.5 ml
AgNO₃ 4/100

Sample	START	finish	=	Δ	
BLK.	0.000	0.001	=	0.001	
STD.	0.010	0.820	=	0.809	
STA	0.850	1.658	=	0.807	
STD.	0.000	0.810	=	0.809	
STA-13	0.840	1.659	=	0.818	19.58
" (0.3ml)	0.000	0.499	=	0.499	cm = .831 19.95 } 19.7
STA-14	0.520	1.344	=	0.823	19.76 19.8
"	0.000	0.825	=	0.824	19.80
STA.	0.850	1.659	=	0.808	
STA-15	0.000	0.810	=	0.809	19.44 19.5
" (0.3ml)	0.830	1.220	=	0.489	cm = .815 19.575
STA-16	0.000	0.867	=	0.866	≥ 20.79 ≤ 20.7
"	0.880	1.744	=	0.863	≤ 20.70
STD.	0.000	0.807	=	0.806	
STD.	0.000	0.806	=	0.805	
STA-17	0.820	1.763	=	0.942	> 21 > 21
"	0.000	0.939	=	0.938	> 21
STA-18	0.960	1.762	=	0.801	19.24 19.3
STD.	0.000	0.806	=	0.805	19.34
STA-19	0.840	1.654	=	0.813	19.54 19.55
"	0.000	0.815	=	0.814	19.56
STA-20	0.830	1.659	=	0.828	19.84 19.8
STA-20	0.000	0.822	=	0.821	19.72
STD.	0.850	1.656	=	0.805	19.34 19.4
STA-21	0.000	0.811	=	0.810	19.46 > 19.4
"	0.830	1.637	=	0.806	19.36
STA-22	0.000	0.820	=	0.819	19.67 19.7
over "	0.850	1.674	=	0.823	19.70

	START	End	A	
STD.	0.000	0.806 =	0.805	
STA.				
23	0.850	1.712 =	0.861 } 0.861	20.49 ⁵
"	0.000	0.862 =	0.861 }	
STA.				
24	0.870	1.690 =	0.819 } 0.817	19.6
"	0.000	0.817 =	0.816 }	
STD.	0.830	1.637 =	0.806	
STA.				
26	0.000	0.816 =	0.815 } 0.818	19.8
"	0.830	1.652 =	0.821 }	
STA.				
27	0.000	0.818 =	0.817 } 0.816	19.6
"	0.830	1.646 =	0.815 }	
STA	1.000	1.810 =	0.809	

Cl⁻

sample + STD. 0.5 ml
AgNO₃ 4/100

79

Hydro Casts @ Piston Core Stations

sample	START	ml's end	Δ			
B/k.	0.000	0.001 =	0.001			
STD.	0.010	0.825 =	0.814			
STA	0.840	1.657 =	0.816			
STD.	0.000	0.813 =	0.812			
STA. 25 4 m	0.830	1.595 =	0.764	18.24	18.30	33.05
"	0.000	0.770 =	0.769	18.36		
STA. 25 8 m	0.790	1.610 =	0.819	19.52	19.51	35.24
"	0.000	0.819 =	0.818	19.50		
STD.	0.830	1.644 =	0.813			
STA. 25 15 m	0.000	0.821 =	0.820	19.54	19.54	35.29
STA 25 25 m	0.840	1.683 =	0.842	20.05	(20.02)	36.16
"	0.000	0.841 =	0.840	20.00		
STD.	0.860	1.670 =	0.809			
STA. 18 6 m	0.000	0.793 =	0.792	18.68	18.92	36.17
"	0.800	1.596 =	0.795	18.96		
STA. 18 10 m	0.000	0.824 =	0.823	19.60	19.60	35.40
"	0.840	1.664 =	0.823	19.60		
STD	0.000	0.814 =	0.813	19.37		
STD	0.000	0.812 =	0.811	19.33		
STA. 13 surf.	0.820	1.591 =	0.770	18.38	18.35	33.14
"	0.000	0.769 =	0.768	18.33		
STA. 13 4 m	0.780	1.554 =	0.773	18.44	18.47	33.36
"	0.000	0.776 =	0.775	18.50		
STD	0.790	1.600 =	0.810	1		
STA. 13 7 m	0.000	0.806 =	0.805	19.10	19.17	34.52
"	0.820	1.624 =	0.803	19.14		
STA. 13 10 m	0.000	0.798 =	0.797	19.00	19.01	34.33
" (0.3 ml)	0.810	1.290 =	0.479	19.02		
STD.	0.000	0.810 =	0.809			
STA. 13 13 m	0.820	1.661 =	0.840	20.00	19.89	35.92
"	0.000	0.832 =	0.831	19.78		
STA. 13 19 m	0.850	1.676 =	0.825	19.65	19.65	(35.45)
STA	1.000	0.814 =	0.813	19.37		

CONVERSION CURVES

TITRATION UNITS — Cl

ASSUMPTION: Density \approx sea water admixtures

Cl₂ (true)

SAMPLES PISTON CORE
STA 17, 16 Not valid
because no calibrating
point in higher range
Need add'l

Sta 13-22

HYDROCASTS

PISTON CORE STA

1-9

$$\begin{array}{r} 812.5 \\ 806.75 \\ \hline 836 \\ 812.5 \\ \hline \end{array} \quad \begin{array}{r} .769 \\ \times \\ \hline .769 \\ \times \\ \hline .769 \\ \times \\ \hline \end{array}$$

$x = .7912$

Cl₂ (true)

20
19
18.0

SAMPLES PISTON CORE
STA 17, 16 Not valid
because no calibrating
point in higher range
Need add l

812.5
806.75
836
812.5
x = .7912

1769
4
3X
1769

Sta 13-22

HYDROCASTS

PISTON CORE STA
1-9

SURF
STA 13

.7 .1 .2 .3 .4 .5 .6 .7 .8 .9 8.0 .1 .2 .3 .4 .5 .6 .7 .8 .9 9.0

Cl₂ + H₂O
reading

GRAPHIC CONTROLS CORPORATION
Buffalo, New York Printed in U.S.A.

GRAPH PAPER



P_p - STA 1. CL - 19.5

P - STA 2. CL - 19.4

PISTON Cores

core
length

22.5' catcher sed. $P = \frac{\text{STA. 3}}{\text{pore H}_2\text{O}}$ S 34.8 CL - 19.5
Surf 36.0

32' catcher sed. $P = \frac{\text{STA. 4}}{\text{pore H}_2\text{O}}$ S 34.7 CL - 19.5
surface 35.6

32' $P = \frac{\text{STA. 5}}{\text{pore H}_2\text{O}}$ S 35.0 CL - 19.5

— NO $\frac{\text{STA. 6}}{\text{sample}}$ — catcher washed out

32' $P = \frac{\text{STA. 7}}{\text{pore water}}$ S = 35.1900 CL - 19.7
— discard

21' $P = \frac{\text{STA. 8}}{\text{pore water}}$ S = 35.3 CL - 19.5

32' $P = \frac{\text{STA. 9}}{\text{pore water}}$ S = 35.5 CL - 19.8

NO $\frac{\text{STA. 10}}{\text{sample saved for pore water}}$ - cc washed

NO $\frac{\text{STA. 11}}{\text{sample}}$ - catcher washed

PISTON CORES (catchers)

6

length ft.

G 80-6

Doyle Line #3

No sample STA 25

STA 26

31'

P = -

pore water

$S_{700} = 35.4$ ^{vial used up} $Cl^- = 19.8$

32'

P = +

STA 27

pore water

$S_{700} = 35.4$ ^{vial used up} $Cl^- = 19.6$

STA 24

pore water

$S_{700} = 35.4$ $Cl^- = 19.6$

STA 23

pore water

$S_{700} = 36.0$ $Cl^- = 20.5$

STA 22

pore water

$S_{700} = 35.8$ $Cl^- = 19.7$

Sta 21

pore H₂O

$S_{700} = 36.3$ ^{vial used up} $Cl^- = 19.4$

STA 20

pore H₂O

$S_{700} = 37.0$ $Cl^- = 19.8$

STA 19

pore H₂O

$S_{700} = 34.3$ $Cl^- = 19.6$

STA 18

pore water

$S_{700} = 32.3$ $Cl^- = 19.3$

26'

P = -

STA 17

$S_{700} (36.7?)$ $Cl^- = > 21$

STA 16

$S_{700} = 37.0$ $Cl^- = \geq 20.7$

16'

P = -

Sta 15

$S_{700} = 34.9$ ^{vial used up} $Cl^- = 19.5$

29'

P = -

core
length ft

Piston Cores (catcher)

G-80-6

~~10~~

35' P = -

STA. 14
pore water

5900 35.3 $CL = 19.8$

STA 13

25' P = -

pore water

5900 = 35.5 $CL = 19.7$ ^{vial used up}

STADridge Sub STD S.W.

IAPSO - 19.376 700 Cl⁻ 35.0037 S C.R. 1.00009IAPSO - null set @ 1.00009 ^{STD} setting 5.58

IAPSO - 1.00019 reset null @ 1.00009 5.63

IAPSO - 1.00024 " " " 5.68

IAPSO - 1.00019 " " " 5.73

IAPSO - 1.00034 " " " 5.835

IAPSO - 1.00029 " " " 5.915

IAPSO - 1.00026 " " " 5.980

IAPSO - 1.00034 " " " 6.080

IAPSO - 1.00016 " " " 6.13

IAPSO - 1.00055

1 min 1.00054

2 min "

5 min "

15 min 1.00053

IAPSO - 1.00129

h h h

h h h

6.66

Sub STD. 0.98344

" " 0.98354

" " 0.98364 - drained

Refill btl. 0.98354 - drained

New STD. 0.98330

671. 0.98360

" 0.98370 - drained

" 0.98376 - drained

" 0.98386 - drained

refill btl. 0.98371 - drained

new STD. 0.98347

" 0.98334

Repeat 0.98360

New STD. 0.98344

New IAPSO water

15
2343

IAPSO	STD.	set	1.00009	null @	4.86
"			1.00016	" "	4.88
"			1.00020		
"	Mix all		1.00046		
"	"		1.00112		

Sub STD. #1

Sm. btl.	{ Sub STD.	0.99594
	" "	0.99590
	" "	0.99590
	→ re use	0.99606
large btl.	Sub STD.	0.99581

Sub STD #2

STD #1	working btl.	0.99593	set null @	0.99590
" "	reserve	0.99590		
" "	"	0.99589		
" "	"	0.99592		
STD #2		1.00160	1.00165	5 35.065
" "		1.00168		
" "		1.00167		

STD #2	working	set @	1.00165	} set null 1.00170
" "	reserve		1.00169	
" "	"		1.00175	
" "	"		1.00174	
STD #3			1.00201	} set null 1.00200
			1.00198	
			1.00200	

KAPSO

Water 27 June 80

Time	R.	S
0403	0.97662	34.08
0615	0.95880	33.38
0715	0.97342	33.95
0805	1.01813	35.70
0910	1.00880	35.34
1010	1.01066	35.43

using sub-std. #1

1120	0.96406	33.58
1630	0.99040	34.62
1750	0.99778	34.91
1840	0.99189	34.68
2000	0.98456	34.39
2200	0.99957	34.98
2300	1.02576	36.01
2348	1.03139	36.23
sub. std.	0.99588	34.83

(34.839)

28 June 80

sub. STA #1

reading 15.6 on meter
↳ null

0027	1.03002	36.18
0125	1.03547	36.40
0230	1.03239	36.27
0415	1.02555	36.00
0520	1.02905	36.14
0640	1.02007	35.79
sub. std.	0.99574 remull	34.833
0825	1.00136	35.05
0940	0.98803	34.52
1050	1.00536	35.21
1140	1.00023	35.00
1313	0.99202	34.68
1405	0.97872	34.16
sub. std.	0.99588	34.838

(34.839)

(34.839)

28 June (cont)

sub. std #1

Time	R.	S	
1456	0.97222	33.91	
1542	0.96734	33.71	
1621	0.96518	33.63	
1702	0.99222	34.69	
1755	1.00977	35.38	
1847	1.01220	35.48	
sub STD.	0.99582	re null	34.836 (34.839)

1920	1.01164	35.45	
1958	1.01658	35.65	
2039	1.02425	35.95	
2122	1.01947	35.76	
2203	1.01057	35.41	
2330	1.01072	35.42	
sub STD.	0.99585	34.837	(34.839)

29 June 80

sub STD #2

0121	1.01538	35.60	
0232	1.00828	35.32	
0306	1.00927	35.36	
0338	1.00831	35.32	
0408	1.01769	35.69	
0520	1.02729	36.07	
sub. std.	1.00204	re null	35.081 (35.065)
0645	0.99949	34.98	
0730	0.96556	35.65	
0835	0.97332	33.95	
0918	0.99228	34.69	
0950	0.99957	34.98	
1025	0.99862	34.94	
sub std	1.00083	re null	35.032 (35.065)

1118	0.98837	34.54	
1147	0.98794	34.52	
1248	0.99898	34.96	
1354	1.00647	35.25	
1513	1.02125	35.83	
1652	1.00344	35.13	

(cont)

29 June (Cont)

58

Sample
~~FAKED~~

Sub std #2

1822

1944

2045

2145

2330

R

1.00160 re null

1.00877

1.00742

0.99307

0.99368

0.99483

F₉₀₀

35.063

35.34

35.29

34.72

34.75

34.79

(35.065)

30 June 80

0057

sub. std #2

0.98722

1.00151

re null

34.49

35.059

(35.065)

0158

0318

0430

0540

0640

0800

0.98711

0.96630

0.99388

0.99067

1.01691

1.00394

34.49

33.67

34.76

34.63

35.66

35.15

sub std #2

1.00141

re null

35.055

(35.065)

0925

1035

1438

1549

1707

1825

1.01199

1.00574

0.98689

0.97795

0.97898

0.98694

35.47

35.22

34.48

34.13

34.17

34.48

sub std #2

1.00155

1.00293

1.00784

1.01298

35.061

35.11

35.30

35.51

(35.065)

1 July 1980

0007

0153

sub std #2

1.00505

1.00742

1.00163

35.19

35.29

35.064

(35.065)

sub std #3

0430

0605

0730

1419 ^{re null}

0.99331

0.99580

0.97465

1.01703

8 35.079

34.73

34.83

34.00

35.66

1 July (cont)

0840	0.96954	33.80
1005	0.98331	34.34
1107	0.98397	34.37
sub std #3	1.00189	35.075
1537	1.01519	35.59
1710	1.01254	35.49
2010	0.98124	34.26
2233	0.98560	34.43

(35.079)

2 July 80

0950	0.98184	34.28
1046	0.99060	34.63
1148	0.99124	34.65
sub std #3	1.00205	35.081

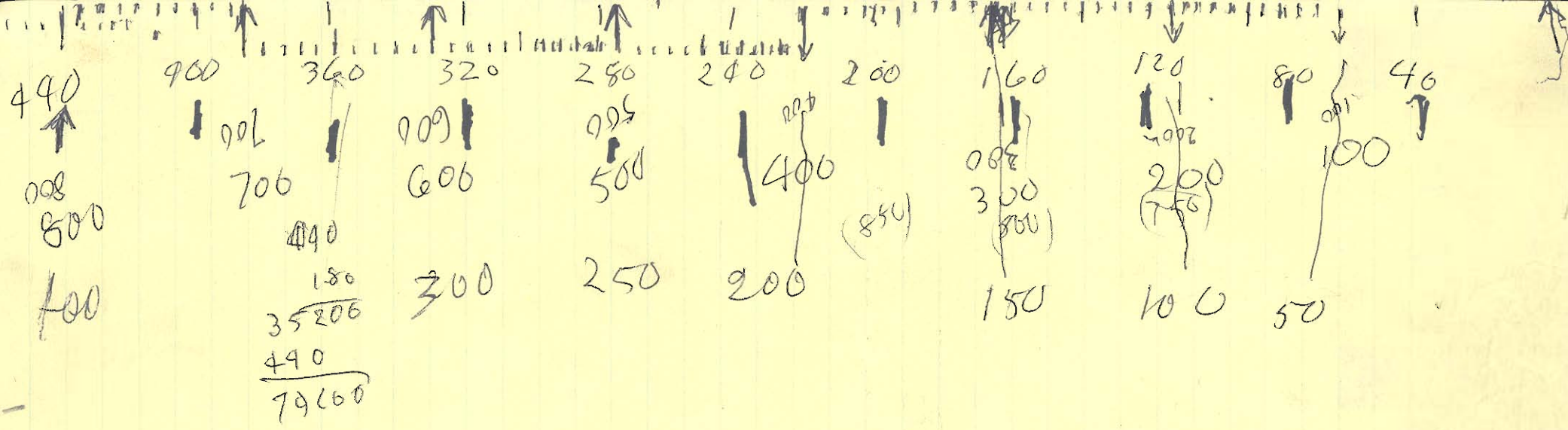
(35.079)

3 July 80

0510	1.01547	35.61
0800	1.02945	36.15
1002	0.99568	34.83
1128	0.99515	34.81

4 July

0055	0.99863	34.94
0225	0.99150	34.66
0600	0.98872	34.53
0645	0.99327	34.73
0730	0.98796	34.52
0830	0.98994	34.60
1005	1.00023	35.00
1144	1.00405	35.15
1430	1.00784	35.30



923 H17 #
 926 - picked up to 2 1/2 km
 932 have to
 12.52

1055 -		45.58 ⁵²		54.15		
1058 -	$\frac{3}{5}$	44.06	87	54.42 ²⁷	45	← 210
1100 -	24	44.71		83	55.00	

1125		42.78		57.13		
1127 -	$\frac{2}{5}$	42.62 ¹⁶	39	57.30 ¹⁷	43	← 465
1130		42.39		57.56		

1130		42.39 ¹⁴		57.56 ¹⁸		
1132	$\frac{2}{5}$	42.25	35	57.38	44	← 620
1135		42.04		58.00		

1140		41.66 ¹⁴		58.45 ¹⁸		
1142	$\frac{2}{5}$	41.52	36	58.63	45	← 765
1145		41.30		58.90		

1145		41.30 ²⁵		58.90		
1147	$\frac{2}{5}$	41.55	63	59.08 ¹⁸	45	← 895
1150		40.93		59.35		

1200		40.25		00.22		
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1435		41.35		83	59.27	Wing 2
→ on Bott		41.30			59.26	- - - Haul 1
1430	24	41.28		83	59.26	

add 4

			Knots	LAT.	Long.
0400-0430	8-8:30	298.6°	0.8	25° 9.95	83° 58.66
0430-0500	8:30-9	210.5°	0.8	25° 9.52	84° 02.59
0500-0530	9-9:30	232.2°	0.5	25° 10.03	84° 06.62
0530-0600	9:30-10	221.2°	0.5	25° 10.03	84° 10.74
0600-0630	10-10:30	222.0°	0.7	25° 10.03	84° 14.87

360.0	360.0
298.6	210.5
<hr/> 61.4°	<hr/> 150.5

Pinger

$$20 \sqrt{4008}$$

$$1.8 \sqrt{400} \sim \text{width}$$

$$20 \sqrt{732}$$

4008 width ~~for~~ Pinger to ball distance

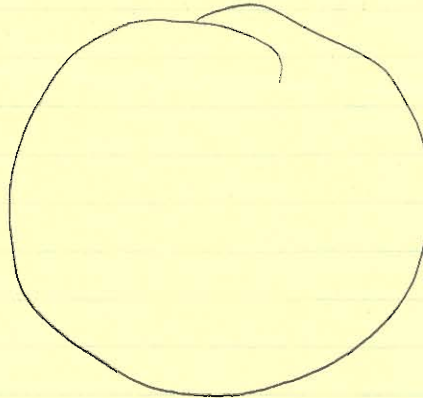
① TURN Bot switch on

2. — 30 min line —

3. Don't use gate; only ping even the time

④ Key on, baseline off 400

⑤ Pinger only 400



4008 = 1 sec

8008 = 2 sec

2000 = 5 sec

Path



Chat speed

Gate timing (programmable)

Length

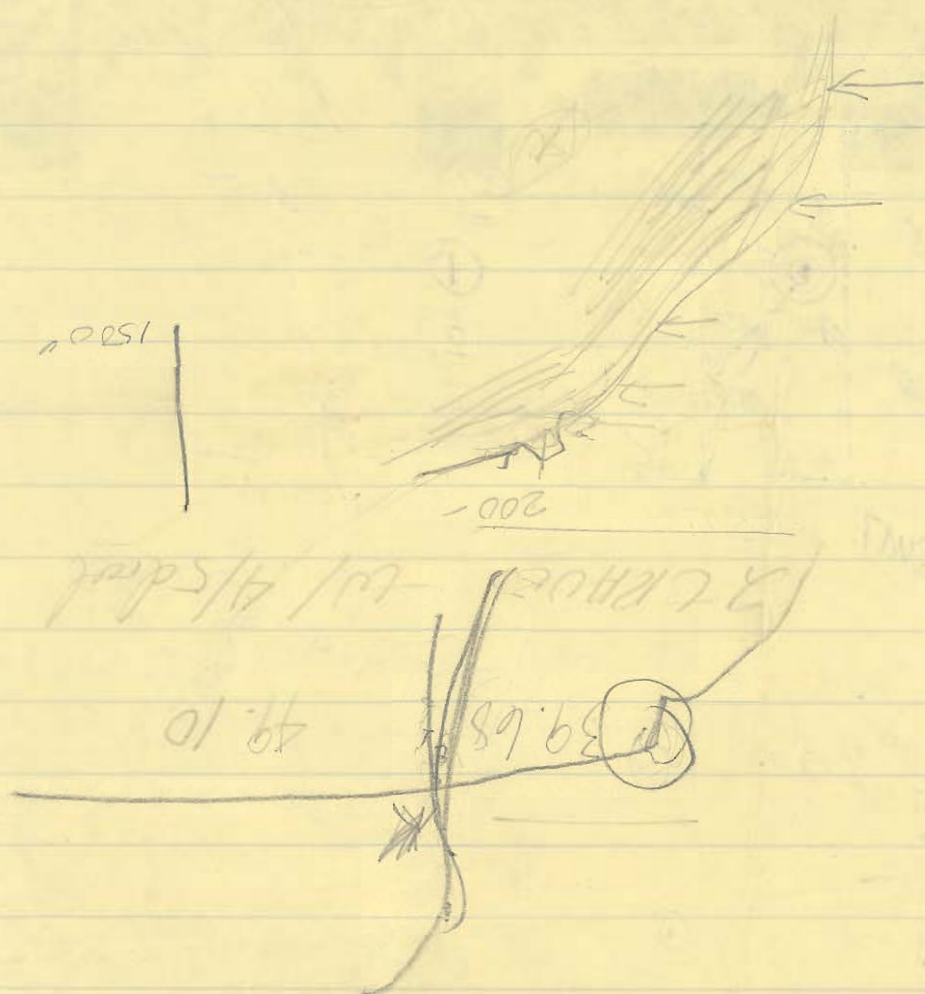
Key pulse

ON

Baseline chf off

ON ON

O O



1700	2nd	4 hrs	Acoustic	2100	4
16 hrs	dredging	1 pm.	3rd.		20
3 hrs	Acoustic	4 pm			23 31.
8 hrs	trawling	3 hauls			12 PM midn.

84 09.2
24 51.4